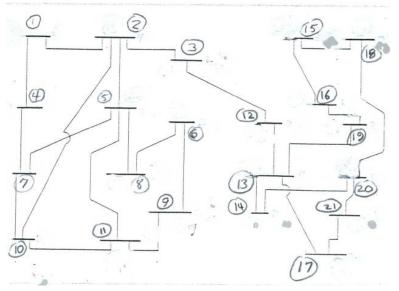
Homework #2, EE 553, Fall 2012, Dr. McCalley, Due Monday, September 17, 2012

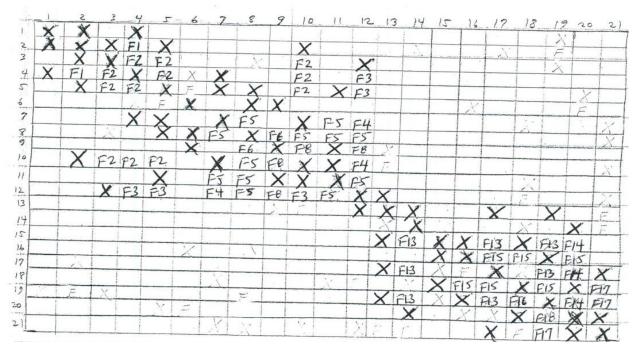
1. Solve for x in the below by hand, using LU-decomposition.

Use BACK SURSTITUTION : X4=1 X3+, 1905 X4=1.1905 > X3=1 X2-,5X3-X4=-,5=) X2=-,5+,5+/= / X, t. 25 X2+. 25 X3 +. 25 X4 = . 75 => X, = D X=

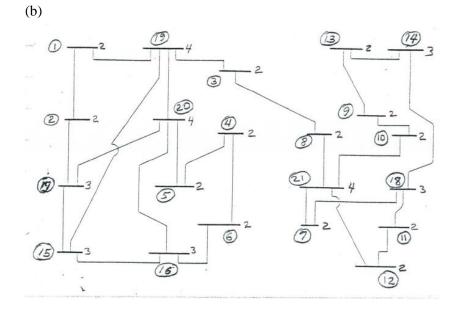
2. Consider the two different numbering systems for the network given below. For each numbering system, determine the number of fill-ups and the number of row operations assuming no re-ordering is performed after the first row operation. Indicate which scheme is better and why. Describe a better scheme.

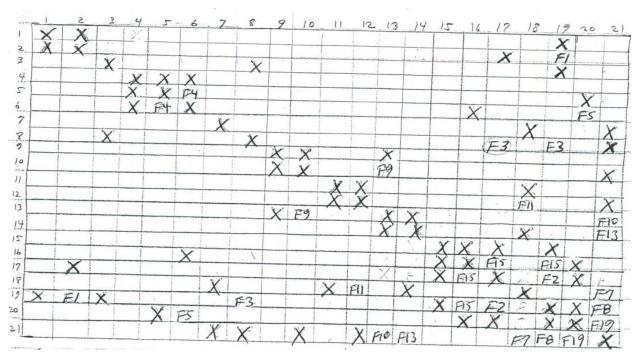
(a)





This scheme has 61 Fill-ups and the elimination procedure will require 55 row operations.

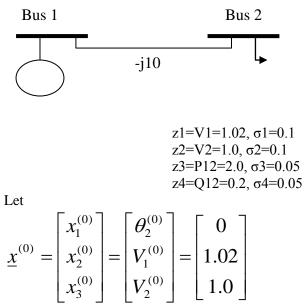




This scheme has 29 fill-ups, and the elimination procedure will require 40 row operations. Since the row number of row operations for this scheme is fewer, it is better than scheme (a).

A better scheme would be to start with scheme (b) and then re-order the buses after each pivot. If we would have applied this, for example, after pivoting on row 1 and getting the fill up in row 2, column 19, we would have then had 3 branches connected to bus 2. Therefore we would have reordered so that bus 2 followed bus 14.

3. For the lossless network shown below, the following data is given:



and perform one iteration of the least squares state estimation solution procedure to find $x^{(1)}$.

1

Now we proceed with the iterative
Let
$$\begin{pmatrix} \hat{\delta}_2^o \\ \hat{\nabla}_1^o \\ \hat{\nabla}_2^o \end{pmatrix} = \begin{pmatrix} 0 \\ 1.02 \\ 1.0 \\ 1.0 \end{pmatrix}$$
5-15

0

0

 $-10V_1V_2\cos \delta_2$

 $10V_1V_2 \sin \delta_2$

e solution process:

1

0

 $20V_1 - 10V_2 \cos \delta_2$

 $-10V_2 \sin \delta_2$

0

1

 $-10V_1 \sin \delta_2$

-10V1cos 82

 $h_4(\delta, v) = 10v_1^2 - 10v_1v_2\cos \delta_2$ The Jacobian Matrix is given by $\begin{cases} \frac{\partial h_1}{\partial \delta_2} & \frac{\partial h_1}{\partial V_1} & \frac{\partial h_1}{\partial V_2} \\ \frac{\partial h_2}{\partial \delta_2} & \frac{\partial h_2}{\partial V_1} & \frac{\partial h_2}{\partial V_2} \\ \frac{\partial h_3}{\partial \delta_2} & \frac{\partial h_3}{\partial V_1} & \frac{\partial h_3}{\partial V_2} \\ \frac{\partial h_4}{\partial \delta_2} & \frac{\partial h_4}{\partial V_1} & \frac{\partial h_4}{\partial V_2} \end{cases}$

 $h_3(\delta, V) = -10V_1V_2 \sin \delta_2$

The vector $h(\delta, V)$ is given by $h_1(\delta, V) = V_1$

 $h_2(\delta, V) = V_2$

 $H(\delta, V) =$

This implies: $z = h(\hat{\delta}^{\circ}, \hat{V}^{\circ}) = \begin{pmatrix} 0 \\ 0 \\ 2.0 \\ -.004 \end{pmatrix}$ $H(\hat{\delta}^{0}, \hat{v}^{c}) = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -10.2 & 0 & 0 \\ 0 & 10 & 1 \end{pmatrix}$ $H^{T}R^{-1}(z - h(\hat{\delta}^{\circ}, \hat{v}^{\circ}))$ $\hat{\delta}^{\circ}, \hat{v}^{\circ})$ $= \begin{pmatrix} 0 & 0 & -10.2 & 0 \\ 1 & 0 & 0 & 10.4 \\ 0 & 1 & 0 & -10 \end{pmatrix} \begin{pmatrix} (.1 \)^{2} & 0 & 0 & 0 \\ 0 & (.1 \)^{2} & 0 & 0 \\ 0 & 0 & (.05)^{2} & 0 \\ 0 & 0 & 0 & (.05)^{2} \end{pmatrix} \begin{bmatrix} 0 \\ 0 \\ 2.0 \\ -.004 \end{pmatrix}$ $= 100 \begin{pmatrix} 0 & 0 & -40.8 & 0 \\ (100)^2 & 0 & 0 & 41.6 \\ 0 & (100)^2 & 0 & -40 \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ 2.0 \\ 0 \end{pmatrix}$ = 100 (-.1664 5-16

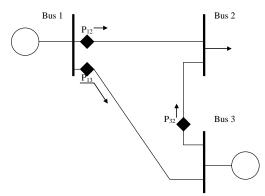
] $H^{T}R^{-1}H = \begin{pmatrix} 0 & 0 & -40.8 & 0 \\ (100)^{2} & 0 & 0 & 41.6 \\ 0 & (100)^{2} & 0 & -40 \end{pmatrix} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ -10.2 & 0 & 0 \\ 0 & 10.4 & -10 \end{pmatrix}$ 1 X 100 (416.16 0 0 -416 433.64 = X 100 0 400 0 -416 As a result we have $\begin{bmatrix} \hat{\delta}_2^1 \\ \hat{v}_1^1 \\ \hat{v}_2^1 \\ \hat{v}_2^1 \end{bmatrix} = \begin{bmatrix} 0 \\ 1.02 \\ 1.0 \end{bmatrix} + \begin{bmatrix} 416.16 & 0 & 0 \\ 0 & 433.64 & 416 \\ 0 & 416 & 400 \end{bmatrix}^{-1} \begin{bmatrix} -.81.6 \\ -.1664 \\ .16 \end{bmatrix}$ (-.1960 1.0203 = 1.000728 From here we proceed to the second iteration, and so on.

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4. Consider the system below. Real power measurements taken as follows: $P_{12}=0.62 \text{ pu}$, $P_{13}=0.06 \text{ pu}$, and $P_{32}=0.37 \text{ pu}$. All voltages are 1.0 per unit, and all measurement devices have $\sigma=0.01$. Assume the bus 3 angle is reference. So the state vector is therefore $\underline{x}=[\theta_1 \ \theta_2]^T$. Your textbook solves this problem using DC power flow equations on pp. 467-471. Repeat, following the indicated steps below, but use AC power flow equations.



- a) Determine the vector of measurement expressions $\underline{h}(\underline{x})$, the derivative expressions $\underline{H} = \frac{\partial \underline{h}(\underline{x})}{\partial \underline{x}}$,
- b) and the weighting matrix <u>R</u>. Compute $\underline{H}(\underline{x}^{(0)})$, $\underline{h}(\underline{x}^{(0)})$ for an estimate of $\underline{x}^{(0)} = [0.024 - 0.093]^T$ (units of radians).

c) Compute
$$\underline{A} = \underline{H}^{T}(\underline{x})\underline{R}^{-1}\underline{H}(\underline{x})\Big|_{\underline{x}^{(0)}}, \ \underline{b} = \underline{H}^{T}(\underline{x})\underline{R}^{-1}[(\underline{z} - \underline{h}(\underline{x}))]_{\underline{x}^{(0)}}$$

d) Solve
$$\underline{A}\Delta \underline{x} = \underline{b}$$
 for $\Delta \underline{x}$.

Solution:

a) Recall series admittance of $g_{pq}+jb_{pq}$; $g_{pq}>0$, $b_{pq}<0$ for inductive line

$$\begin{aligned} h_i(\underline{x}) &= P_{p,inj} = \sum_{k=1}^n \left| V_p \right| \left| V_k \right| \left(G_{pk} \cos(\theta_p - \theta_k) + B_{pk} \sin(\theta_p - \theta_k) \right) = 0 \\ h_1(\underline{x}) &= P_{12} = \left| V_1 \right|^2 g_{12} - \left| V_1 \right| \left| V_2 \right| g_{12} \cos(\theta_1 - \theta_2) - \left| V_1 \right| \left| V_2 \right| b_{12} \sin(\theta_1 - \theta_2) = 5 \sin(\theta_1 - \theta_2) \\ h_2(\underline{x}) &= P_{13} = \left| V_1 \right|^2 g_{12} - \left| V_1 \right| \left| V_3 \right| g_{13} \cos(\theta_1 - \theta_3) - \left| V_1 \right| \left| V_3 \right| b_{13} \sin(\theta_1 - \theta_3) = 2.5 \sin(\theta_1 - \theta_3) \\ &= 2.5 \sin(\theta_1) \\ h_3(\underline{x}) &= P_{32} = \left| V_3 \right|^2 g_{32} - \left| V_3 \right| \left| V_2 \right| g_{32} \cos(\theta_3 - \theta_2) - \left| V_3 \right| \left| V_2 \right| b_{32} \sin(\theta_3 - \theta_2) = 4 \sin(\theta_3 - \theta_2) \\ &= 4 \sin(-\theta_2) = -4 \sin(\theta_2) \end{aligned}$$

$$\underbrace{H} = \frac{\partial h(x)}{\partial x} = \begin{bmatrix} \frac{\partial h_1(x)}{\partial x_1} & \frac{\partial h_1(x)}{\partial x_2} \\ \frac{\partial h_2(x)}{\partial x_1} & \frac{\partial h_2(x)}{\partial x_2} \\ \frac{\partial h_3(x)}{\partial x_1} & \frac{\partial h_3(x)}{\partial x_2} \end{bmatrix} = \begin{bmatrix} \frac{\partial P_{12}(x)}{\partial \theta_1} & \frac{\partial P_{13}(x)}{\partial \theta_2} \\ \frac{\partial P_{13}(x)}{\partial \theta_1} & \frac{\partial P_{13}(x)}{\partial \theta_2} \\ \frac{\partial P_{32}(x)}{\partial \theta_1} & \frac{\partial P_{32}(x)}{\partial \theta_2} \end{bmatrix} = \begin{bmatrix} 5\cos(\theta_1 - \theta_2) & -5\cos(\theta_1 - \theta_2) \\ 2.5\cos(\theta_1) & 0 \\ 0 & -4\cos(\theta_2) \end{bmatrix} \\
\underbrace{R} = \begin{bmatrix} \sigma_1^2 & 0 & \cdots & 0 \\ 0 & \sigma_2^2 & 0 & 0 \\ \vdots & 0 & \ddots & 0 \\ 0 & 0 & 0 & \sigma_m^2 \end{bmatrix} = \begin{bmatrix} 0.0001 & 0 & 0 \\ 0 & 0.0001 & 0 \\ 0 & 0.0001 & 0 \\ 0 & 0 & 0.0001 \end{bmatrix} \\
b) \text{ With } \underline{x}^{(0)} = [0.024 & -0.093]^{\mathrm{T}}, \underbrace{H(x^{(0)})}_{0}, \underbrace{h(x^{(0)})}_{0} \text{ become:} \\
h_1(x) = P_{12} = 5\sin(\theta_{\Gamma} - \theta_2) = 5\sin(0.024 + 0.093) = 0.5837 \\
h_2(x) = P_{13} = 2.5\sin(\theta_{\Gamma}) = 2.5\sin(0.024) = 0.06 \\
h_3(x) = P_{32} = -4\sin(\theta_2) = -4\sin(-.093) = 0.3715 \\
\underbrace{H} = \begin{bmatrix} 5\cos(\theta_1 - \theta_2) & -5\cos(\theta_1 - \theta_2) \\ 2.5\cos(\theta_1) & 0 \\ 0 & -4\cos(\theta_2) \end{bmatrix} = \begin{bmatrix} 5\cos(0.024 + 0.093) & -5\cos(0.024 + 0.093) \\ 2.5\cos(0.024) & 0 \\ 0 & -4\cos(-0.093) \end{bmatrix} = \begin{bmatrix} 4.9658 & -4.9658 \\ 2.4993 & 0 \\ 0 & -3.9827 \end{bmatrix}$$

$$\underline{A} = \underline{H}^{T}(\underline{x})\underline{R}^{-1}\underline{H}(\underline{x})\Big|_{\underline{x}^{(0)}} = \begin{bmatrix} 4.9658 & 2.4993 & 0\\ -4.9658 & 0 & -3.9827 \end{bmatrix} \begin{bmatrix} 0.0001 & 0 & 0\\ 0 & 0.0001 & 0\\ 0 & 0 & 0.0001 \end{bmatrix}^{-1} \begin{bmatrix} 4.9658 & -4.9658\\ 2.4993 & 0\\ 0 & -3.9827 \end{bmatrix} \\ = \begin{bmatrix} 4.9658 & 2.4993 & 0\\ -4.9658 & 0 & -3.9827 \end{bmatrix} \begin{bmatrix} 10000 & 0 & 0\\ 0 & 10000 & 0\\ 0 & 0 & 10000 \end{bmatrix} \begin{bmatrix} 4.9658 & -4.9658\\ 2.4993 & 0\\ 0 & -3.9827 \end{bmatrix} = \begin{bmatrix} 309060 & -246590\\ -246590 & 405210 \end{bmatrix}$$

$$\begin{split} \underline{b} &= \underline{H}^{T}(\underline{x})\underline{R}^{-1}[(\underline{z} - \underline{h}(\underline{x}))]_{\underline{x}^{(0)}} \\ &= \begin{bmatrix} 4.9658 & 2.4993 & 0 \\ -4.9658 & 0 & -3.9827 \end{bmatrix} \begin{bmatrix} 10000 & 0 & 0 \\ 0 & 10000 & 0 \\ 0 & 0 & 10000 \end{bmatrix} \begin{bmatrix} 0.62 - 0.5837 \\ 0.06 - 0.06 \\ 0.37 - 0.3715 \end{bmatrix} \\ &= \begin{bmatrix} 4.9658 & 2.4993 & 0 \\ -4.9658 & 0 & -3.9827 \end{bmatrix} \begin{bmatrix} 10000 & 0 & 0 \\ 0 & 10000 & 0 \\ 0 & 0 & 10000 \end{bmatrix} \begin{bmatrix} 0.0363 \\ 0 \\ -0.0015 \end{bmatrix} = \begin{bmatrix} 1802.6 \\ -1742.8 \end{bmatrix} \\ d \end{split}$$

$$\begin{aligned} d \\ &= \begin{bmatrix} 309060 & -246590 \\ -246590 & 405210 \end{bmatrix} \begin{bmatrix} \Delta\theta_{1} \\ \Delta\theta_{2} \end{bmatrix} = \begin{bmatrix} 1802.6 \\ -1742.8 \end{bmatrix} \Rightarrow \begin{bmatrix} \Delta\theta_{1} \\ \Delta\theta_{2} \end{bmatrix} = \begin{bmatrix} 0.0047 \\ -.0015 \end{bmatrix} \\ &\text{And the new value of } \underline{x} \text{ would then be} \\ &= \begin{bmatrix} \theta_{1} & \theta_{2} \end{bmatrix}^{T} = \begin{bmatrix} 0.024 & -0.093 \end{bmatrix}^{T} + \begin{bmatrix} .0047 & -.0015 \end{bmatrix}^{T} = \begin{bmatrix} 0.0287 & -.0945 \end{bmatrix} \end{aligned}$$

5. Work problem 12.3 in your W&W textbook.

Solution:

a) Let the state vector be
$$\begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix}$$

-Then
H = $\begin{bmatrix} 4 & -4 & 0 \\ 4 & 0 & -2 \\ -2 & 0 & 2 \end{bmatrix}$ R = $\begin{bmatrix} (.02)^2 \\ (.01)^2 \\ (.01)^2 \end{bmatrix}$
Note: The order of the measurements in the H matrix is m_{12} , m_{13} ,
m₃₁
[H^TR⁻¹H] = $\begin{bmatrix} 4 & 2 & -2 \\ -4 & 0 & 0 \\ 0 & -2 & 2 \end{bmatrix}$ $\begin{bmatrix} 2500 \\ 10000. \\ 10000. \end{bmatrix}$ $\begin{bmatrix} 4 & -4 & 0 \\ 2 & 0 & -2 \\ -2 & 0 & 2 \end{bmatrix}$
= $\begin{bmatrix} 10,000. & 20,000. & -20,000. \\ -10,000. & 0 & - \\ 0 & -20,000. & 20,000. \end{bmatrix}$ $\begin{bmatrix} 4 & -4 & 0 \\ 2 & 0 & -2 \\ -2 & 0 & 2 \end{bmatrix}$
= $\begin{bmatrix} 120,000. & -40,000. & -80,000. \\ -40,000. & 40,000. & 0 \\ -80,000. & 0 & 80,000. \end{bmatrix}$

This matrix is singular thus indicating that the network is unobservable. b) With the new measurement:

$$P_{3} = P_{31} + P_{34} = 4(\theta_{3}-\theta_{1}) + 10(\theta_{3}-\theta_{4})$$

$$= 14\theta_{3} - 4\theta_{1}$$
Then $H = 12\begin{bmatrix} 4 & -4 & 0 \\ 2 & 0 & -2 \\ -3 & -2 & 0 & 2 \\ -4 & 0 & 14 \end{bmatrix} = \begin{bmatrix} (.02)^{2} & ... \\ (.01)^{2} & ... \\ (.015)^{2} \end{bmatrix}$

$$[H^{T}R^{-1}H] = \begin{bmatrix} .19111 \cdot 10^{6} & -.4 \cdot 10^{5} & -.32889 \cdot 10^{6} \\ -4 \cdot 10^{5} & .4 \cdot 10^{5} & 0 \\ ... & .32889 \cdot 10^{6} & 0 & .95111 \cdot 10^{6} \end{bmatrix}$$

$$[H^{T}R^{-1}H]^{-1} = \begin{bmatrix} .2675 \cdot 10^{-4} & .2675 \cdot 10^{-4} & .925 \cdot 10^{-5} \\ .2675 \cdot 10^{-4} & .5175 \cdot 10^{-4} & .925 \cdot 10^{-5} \\ .925 \cdot 10^{-5} & .925 \cdot 10^{-5} & .425 \cdot 10^{-5} \end{bmatrix}$$

$$\begin{bmatrix} \theta_{1}^{est} \\ \theta_{2}^{est} \\ \theta_{3}^{est} \\ \theta_{4}^{est} \end{bmatrix} = \begin{bmatrix} -.407 \\ -.460 \\ -.051 \\ 0 \end{bmatrix}$$

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The estimated flows are shown below:

